Heat & Mass Flow Processes

Week_04

Instructor: Mr. Adnan Qamar

Mechanical Engineering Department

> Let us consider a small element of a sphere as shown in Fig. 1 in which heat flows in all three directions r, θ , and ϕ as shown in Fig. below;

Coordinates:	r	•	θ	:	φ
Heat Transfer:	Qr	:	Qθ	:	Qφ
Heat Flux (q=Q/A)	qr	:	$q\theta$:	qø
Thickness:	dr	:	rdθ	:	rsinθ dφ





- Energy balance for the small element is obtained from the First law of Thermodynamics.
 - (Net heat conducted into the element in dr, $rd\theta$, $rsin\theta d\phi$ per unit time I) + (Internal heat generated per unit time II)
 - = (Increase in internal energy per unit time III) + (work done by element per unit time IV)
- The IV term is small because the work done by the element due to change in temperature in neglected.

Qin–Qout + Qgen. = Rate of change in Internal Energy

$$\frac{\text{Heat Diffusion Equation in Spherical Coordinate System}}{(Q_r + Q_{\theta} + Q_{\phi}) - (Q_{r+dr} + Q_{\theta+d\theta} + Q_{\phi+d\phi}) + (Qgen.)} = mc \frac{\partial T}{\partial \tau}$$
$$(Q_r + Q_{\theta} + Q_{\phi}) - (Q_{r+dr} + Q_{\theta+d\theta} + Q_{\phi+d\phi}) + (Qgen.) = \rho vc \frac{\partial T}{\partial \tau} \rightarrow (1)$$

Let

- ▷ Q_r be the heat flux in "r" direction at face AECG and Q_{r+dr} be the heat flux at r+dr direction at face BDFH.
- ► Q_{θ} be the heat flux in " θ " direction at face ABCD and $q_{\theta+d\theta}$ be the heat flux at $\theta+d\theta$ direction at face EFGH.
- ▷ Q_{ϕ} be the heat flux in " ϕ " direction at face DHCG and $Q_{\phi+d\phi}$ be the heat flux at $\phi+d\phi$ direction at face AEBF

Heat Diffusion Equation in Spherical Coordinate System
Now the rate of heat transfer in 'r', '
$$\theta$$
', and ' ϕ ' direction is given by:
 $Q_r = -k.r^2 d\theta \sin \theta d\phi \frac{\partial T}{\partial r}; Q_{r+dr} = Q_r + \frac{\partial}{\partial r} (Q_r) dr + \dots$
 $Q_{\theta} = -k.rdr \sin \theta d\phi \frac{\partial T}{rd\theta}; Q_{\theta+d\theta} = Q_{\theta} + \frac{\partial}{\partial \theta} (Q_{\theta}) d\theta + \dots$
 $Q_{\phi} = -k.rd\theta dr \frac{dT}{r\sin \theta d\phi}; Q_{\phi+d\phi} = Q_{\phi} + \frac{\partial}{\partial \phi} (Q_{\phi}) d\phi + \dots$

Now by putting all values in Equation (1) we have.

$$\begin{split} &-\frac{\partial}{\partial r}(\mathcal{Q}_{r})dr - \frac{\partial}{\partial \theta}(\mathcal{Q}_{\theta})d\theta - \frac{\partial}{\partial \phi}(\mathcal{Q}_{\phi})d\phi + q^{\prime\prime\prime}N = \rho Vc\frac{\partial T}{\partial \tau} \\ &-\frac{\partial}{\partial r}(-k.r^{2}d\theta\sin\theta d\phi\frac{\partial T}{\partial r})dr - \frac{\partial}{\partial \theta}(-k.rdr\sin\theta d\phi\frac{\partial T}{r\partial \theta})d\theta \\ &-\frac{\partial}{\partial \phi}(-k.rd\theta dr\frac{\partial T}{r\sin\theta\partial \phi})d\phi + q^{\prime\prime\prime}N = \rho Vc\frac{\partial T}{\partial \tau} \\ &k.drd\theta d\phi\sin\theta\frac{\partial}{\partial r}\left[r^{2}\frac{\partial T}{\partial r}\right] + k.drd\theta d\phi\frac{\partial}{\partial \theta}\left[\sin\theta d\phi\frac{\partial T}{\partial \theta}\right] \\ &+\frac{k.drd\theta d\phi}{\sin\theta}\frac{\partial}{\partial \phi}\left[\frac{\partial T}{\partial \phi}\right] + q^{\prime\prime\prime}N = \rho Vc\frac{\partial T}{\partial \tau} \end{split}$$

Since volume=v=dr.rd θ .rsin θ d ϕ , hence by dividing both sides of the above equation by "k.V", it is obtained that;

$$\frac{1}{r^{2}} \cdot \frac{\partial}{\partial r} \left[r^{2} \frac{\partial T}{\partial r} \right] + \frac{1}{r^{2} \sin \theta} \cdot \frac{\partial}{\partial \theta} \left[\sin \theta \frac{\partial T}{\partial \theta} \right] \\ + \frac{1}{r^{2} \sin^{2} \theta} \cdot \frac{\partial}{\partial \phi} \left(\frac{\partial T}{\partial \phi} \right) + \frac{q'''}{k} = \frac{1}{\alpha} \cdot \frac{dT}{d\tau} \to (2)$$

This equation is called unsteady state equation for spherical coordinate system.

- \Rightarrow Consider a hollow sphere, whose inside and outside radii are r_i and r_0 respectively.
- ☆ Inner and outer surfaces are maintained at temp T_i and T_0 with uniform thermal conductivity k.



Assume no heat generation, steady state, temperature variation only in radial direction. From general heat conduction equation;

$$\frac{1}{r^{2}} \cdot \frac{\partial}{\partial r} [r^{2} \frac{\partial T}{\partial r}] + \frac{1}{r^{2} \sin \theta} \cdot \frac{\partial}{\partial \theta} [\sin \theta \frac{\partial T}{\partial \theta}] + \frac{1}{r^{2} \sin^{2} \theta} \cdot \frac{\partial}{\partial \phi} (\frac{\partial T}{\partial \phi}) + \frac{q'''}{k} = \frac{1}{\alpha} \cdot \frac{dT}{d\tau} \to (3)$$

Hence, equation (3) can be written as in terms of radius "r";

$$\left[\frac{\partial^2 T}{\partial r^2} + \frac{2}{r}\frac{\partial T}{\partial r} + \frac{q'''}{k} = \frac{1}{\alpha} \cdot \frac{\partial T}{\partial \tau}\right] \longrightarrow (4)$$

Now heat conduction equation becomes.

$$\frac{\partial^2 T}{\partial r^2} + \frac{2}{r} \cdot \frac{\partial T}{\partial r} = o$$

Multiply by r^2 throughout, we get

$$r^{2}\frac{d^{2}T}{dr^{2}} + 2r \cdot \frac{dT}{dr} = 0$$

(or) $\frac{d}{dr}\left(r^{2} \cdot \frac{dT}{dr}\right) = 0$
Hence $\frac{d}{dr}\left(r^{2}\frac{dT}{dr}\right) = 0$

Integrating the above equation,

$$r^2 \cdot \frac{dT}{dr} = C_1$$
$$\frac{dT}{dr} = \frac{C_1}{r^2}$$

Integrating again

....

. .

$$T = -\frac{C_1}{r} + C_2 \quad \longrightarrow \quad (5)$$

To find C_1 and C_2 apply boundary conditions

$$T = T_i \quad \text{at} \quad r = r_i \quad \therefore \quad T_i = -\frac{C_1}{r_i} + C_2 \quad \rightarrow (6)$$
$$T = T_0 \quad \text{at} \quad r = r_0 \quad \therefore \quad T_0 = -\frac{C_1}{r_0} + C_2 \quad \rightarrow (7)$$

Solving for C_1 and C_2

· .

. · .

$$C_{1} = \frac{T_{i} - T_{0}}{\left(\frac{1}{r_{0}} - \frac{1}{r_{i}}\right)} \qquad \therefore \qquad C_{2} = T_{i} + \frac{1}{r_{i}} \frac{(T_{i} - T_{0})}{\left(\frac{1}{r_{0}} - \frac{1}{r_{i}}\right)}$$
$$T = \frac{T_{i} - T_{0}}{\left(\frac{1}{r_{0}} - \frac{1}{r_{i}}\right)r} + \left(T_{i} + \frac{1}{r_{i}} \frac{(T_{i} - T_{0})}{\left(\frac{1}{r_{0}} - \frac{1}{r_{i}}\right)}\right)$$
$$T = T_{i} - \frac{T_{i} - T_{0}}{\left(\frac{1}{r_{0}} - \frac{1}{r_{i}}\right)} \left(\frac{1}{r} - \frac{1}{r_{i}}\right) \rightarrow (8)$$

T is called temperature distribution for hollow sphere.

To find heat flow,

$$Q = -kA \cdot \frac{dT}{dr} = -k \cdot 4\pi r^2 \cdot \frac{dT}{dr}$$

$$Q\cdot\frac{dr}{r^2}=-k4\pi\cdot dT$$

Integrating the above equation

$$Q \int_{r_{i}}^{r_{0}} \frac{dr}{r^{2}} = -4\pi k \int_{T_{i}}^{T_{0}} dT$$
$$-Q \left[\frac{1}{r_{0}} - \frac{1}{r_{i}} \right] = -4\pi k (T_{0} - T_{i})$$
$$-Q \left[\frac{r_{i} - r_{0}}{r_{0}r_{i}} \right] = -4\pi k (T_{0} - T_{i})$$
$$Q = \frac{4\pi k r_{0}r_{i}(T_{i} - T_{0})}{r_{0} - r_{i}} \rightarrow (9)$$

Thermal resistance for a spheral system is

$$R_{\text{th. sp.}} = \frac{r_0 - r_i}{4\pi k r_0 r_i}$$

 \rightarrow (10)

- ☆ Let us consider a sphere of radius R and uniform thermal conductivity k.
- \therefore Consider an elemental ring of radius r and thickness dr. Heat generated in dr is Q_g .
- ☆ Let us electric current is pass through the sphere, causes uniform that generation within the sphere.
- ☆ Let the surface temperature of the sphere be T_w . Heat generated in the sphere be $q'''W/m^3$.

From general heat conduction equation;

$$\frac{1}{r^{2}} \cdot \frac{\partial}{\partial r} \left[r^{2} \frac{\partial T}{\partial r} \right] + \frac{1}{r^{2} \sin \theta} \cdot \frac{\partial}{\partial \theta} \left[\sin \theta \frac{\partial T}{\partial \theta} \right] + \frac{1}{r^{2} \sin^{2} \theta} \cdot \frac{\partial}{\partial \phi} \left(\frac{\partial T}{\partial \phi} \right) + \frac{q'''}{k} = \frac{1}{\alpha} \cdot \frac{dT}{d \tau} \rightarrow (11)$$



Since there is steady state conduction in radial direction only with internal heat generation, all the other terms will become equal to zero. Hence equation (14) will become;

$$\frac{1}{r^2} \cdot \frac{\partial}{\partial r} \left[r^2 \frac{\partial T}{\partial r} \right] + \frac{q^{\prime\prime\prime}}{k} = 0 \Longrightarrow \frac{\partial}{\partial r} \left[r^2 \frac{\partial T}{\partial r} \right] + \frac{q^{\prime\prime\prime} r^2}{k} = 0 \Longrightarrow \frac{d}{dr} \left[r^2 \frac{dT}{dr} \right] + \frac{q^{\prime\prime\prime} r^2}{k} = 0 \to (12)$$

Integrating the above equation

$$r^2 \cdot \frac{dT}{dr} = -\frac{q'''r^3}{3k} + C_1$$

agam megrating we get,

$$\int \frac{dT}{dr} = -\frac{q'''}{3k} \int \frac{r^3}{r^2} + \int \frac{C_1}{r^2}$$

$$T = -\frac{q'''r^2}{6k} - \frac{C_1}{r} + C_2 \longrightarrow (13)$$

To find C_1 and C_2 Apply Boundary Cor.

i.
$$\frac{dT}{dr} = 0$$
 at $r = 0$

ii. $T = T_w$ at r = R

By first boundary condition

$$C_1 = 0$$

Now equation 5 becomes,

$$T = -\frac{q'''r^2}{6k} + C_2$$

apply boundary condition (ii)

$$T_2 = -\frac{q'''R^2}{6k} + C_2$$
$$C_2 = T_w + \frac{q'''R^2}{6k}$$

Substituting C_1 and C_2 in equation (13), we get

$$T = T_w + \frac{q'''}{6k} (R^2 - r^2)$$
$$T = T_w + \frac{q'''}{6k} R^2 \left[1 - \left(\frac{r}{R}\right)^2 \right] \to (14)$$

At centre temperature $T = T_c$ and r = 0

$$T_c = T_w + \frac{q'''R^2}{6k}$$

centre temperature T_c is also called Maximum Temperature

$$T_{\max} = T_w + \frac{q''' R^2}{6k} \longrightarrow (15)$$

To find wall or surface temperature Heat generated in the sphere

$$(Q) = V \times q'''$$

V: Volume
$$Q = \frac{4}{3}\pi R^3 \cdot q''' \rightarrow (16)$$

Heat transfer due to convection on the surface of the sphere

$$Q = h A(T_w - T_\infty)$$
$$Q = h 4\pi R^2 (T_w - T_\infty) \rightarrow (17)$$

<u>Heat Conduction Through a Sphere with Internal Generation</u> Equating equation (16) and (17);

$$\frac{4}{3}\pi R^3 \cdot q''' = 4\pi R^2 h(T_w - T_\infty)$$

$$T_w = T_\infty + \frac{q'''R}{3h} \to (18)$$

where,

 T_w : surface temperature of the sphere.

Example 4.1:

A hollow sphere 10 cm I.D and 30 Cm O.D of a material having thermal conductivity 50 W/mK is used as a container for a liquid chemical mixture. Its inner and outer surface temperatures are 300^0 C and 100^0 C respectively. Determine the heat flow rate through the sphere. Also estimate the temperature at a point quarter of the way between inner and outer surface.

Solution

$$Q = \frac{4\pi r_o r_i k (T_i - T_o)}{(r_o - r_i)} = \frac{(12.56)(0.15)(0.05)(50)(300 - 100)}{(0.15 - 0.05)}$$
$$Q = 9.42kW$$

The value of r at one-fourth way of inner and outer surface is

:. r = 7.5cm :. Temperature at r = 7.5cm i.e., $5 + \frac{1}{4}(15-5) = 7.5cm$

$$T = \frac{r_o}{r} \frac{(r - r_i)}{(r_o - r_i)} (T_o - T_i) + T_i$$

i.e.,
$$\frac{4\pi k r_i r_o (T_i - T_o)}{r_o - r_i} = \frac{4\pi k r r_i (T - T_i)}{r - r_i}$$
$$T = \frac{r_o}{r} \frac{(r - r_i)}{(r_o - r_i)} (T_o - T_i) + T_i$$
$$T = \frac{0.15}{0.075} \frac{(0.075 - 0.05)}{(0.15 - 0.05)} (100 - 300) + 300 = 200^\circ C$$

Example 4.2:

The average heat produced by oranges ripening is estimated to be 300 W/m^2 . Taking the average size of an orange to be 8 cm and assuming it to be a sphere, with k = 0.15 W/mK, calculate the temperature at the centre of the orange.

Given:

$$Q/A = 300 W/m^2$$
$$D = 8 cm = 0.08 n$$
$$R = 0.04 m$$
$$k = 0.15 W/mK$$

Find:

 T_{\max}

Solution

We know that,

$$\frac{Q}{A} = q''' \times \frac{Volume}{Area}$$
$$= \frac{q''' \times 4/3\pi R^3}{4\pi R^2}$$
$$\frac{Q}{A} = \frac{q'''}{3}R$$
$$\therefore q''' = \frac{3Q}{AR}$$
$$= \frac{3 \times 300}{0.04}$$

Heat generated |q'|

$$''' = 2.25 \times 10^4 \ W/m^3$$

... Temperature at the center of the sphere

$$T_{\max} = T_{\infty} + \frac{q''' R^2}{6k}$$
$$= 10 + \frac{2.25 \times 10^4 (0.04)^2}{6 \times 0.15}$$

$$T_{\rm max} = 50^{\circ}C$$

Links for Video Lectures

Theory Class:

https://pern.sharepoint.com/sites/HMFP-MECH-TECH-2018/Shared%20Documents/General/Recordings/HMFP%20THEORY-20210502_101529-Meeting%20Recording.mp4?web=1

Lab Session_04:

https://pern.sharepoint.com/sites/HMFP-MECH-TECH-2018/Shared%20Documents/General/Recordings/HMFP%20LAB-20210502_123847-Meeting%20Recording.mp4?web=1

